

Sky Reconstruction from Cylinder Visibilities

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Visibility

This note will consider the reconstruction of the sky from the measured visibilities from a pair of cylinder antenna arrays. It is assumed that the cylinders fixed and are oriented along the meridian. Each cylinder is populated with \mathbf{N} feeds spaced uniformly along the length. The output voltage of each feed provides an input of a spatial Fourier transform along the cylinder length. The spatial Fourier transform forms \mathbf{N} beams along the length of the cylinder.

For a pair of cylinders the visibility between cylinders is formed for each beam. As the sky drifts through the cylinder beam, the visibility for beam \mathbf{k} is:

$$v_k(\varphi) = \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \frac{\tilde{A}_k(\theta, \phi)}{\lambda^2} T(\theta, \varphi - \phi) \cos(\theta) d\theta d\phi \quad (1)$$

Where φ is the time of the day (in units of angle), λ is the wavelength and \mathbf{T} is the power flux of the sky. The cylinder pair Fourier area is defined as

$$\tilde{A}_k(\theta, \phi) = \tilde{a}_{k,c1}(\theta, \phi) \left(\tilde{a}_{k,c2}(\theta, \phi) \right)^* \quad (2)$$

where the subscripts $\mathbf{c1}$, $\mathbf{c2}$ indicate cylinder 1 and cylinder 2, respectively. The Fourier root area of a cylinder is defined as

$$\tilde{a}_{k,c}(\theta, \phi) = \sum_n a_n(\theta, \phi) e^{-j\vec{\beta}(\theta, \phi) \cdot \vec{r}_{n,c}} e^{j2\pi k \frac{n}{N}} \quad (3)$$

Where \mathbf{n} is the feed number, $\mathbf{r}_{n,c}$ is the global location of the feed and $\vec{\beta}$ is the incoming wave vector:

$$\vec{\beta}(\theta, \phi) = \frac{2\pi}{\lambda} (\sin(\theta)\hat{x} + \cos(\theta)\sin(\phi)\hat{y}) \quad (4)$$

It is assumed that the length of the cylinders is in the x direction.

Sky Expansion

Since the sky is periodic, it can be expanded in a Fourier series:

$$T_c(\theta, \phi) = \sum_l \sum_m \hat{T}_{m,l} e^{jl\pi\sin(\theta)} e^{jm\phi} \quad (5)$$

Since T_c is a complex function but the sky temperature must be a real function, the sky temperature can be written as:

$$T(\theta, \phi) = T_c(\theta, \phi) + (T_c(\theta, \phi))^* \quad (6)$$

$$T(\theta, \phi) = \sum_l \sum_m \hat{T}_{m,l} e^{jl\pi \sin(\theta)} e^{jm\phi} + \sum_l \sum_m (\hat{T}_{m,l})^* e^{-jl\pi \sin(\theta)} e^{-jm\phi} \quad (7)$$

$$T(\theta, \phi) = \sum_l \sum_m (\hat{T}_{m,l} + (\hat{T}_{-m,-l})^*) e^{jl\pi \sin(\theta)} e^{jm\phi} \quad (8)$$

Substituting Equation 8 into Equation 1,

$$v_k(\varphi) = \sum_l \sum_m (\hat{T}_{m,l} + (\hat{T}_{-m,-l})^*) e^{jm\varphi} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \frac{\tilde{A}_k(\theta, \phi)}{\lambda^2} e^{jl\pi \sin(\theta)} e^{-jm\phi} \cos(\theta) d\theta d\phi \quad (9)$$

Fourier Transform of Cylinder Visibilities

Now assume that the visibility is measured at N discrete times during the day. The visibility will be periodic with a period of a day so we can expand the visibility into a Fourier series.

$$v_k(\varphi_n) = \sum_{m'} \tilde{V}_{k,m'} e^{jm\varphi_n} \quad (10)$$

where

$$\tilde{V}_{k,m'} = \frac{1}{N} \sum_n v_k(\varphi_n) e^{-jm\varphi_n} \quad (11)$$

Substituting Equations 9 into Equations 11,

$$\tilde{V}_{k,m} = \sum_l \hat{A}_{k,l,m} (\hat{T}_{m,l} + (\hat{T}_{-m,-l})^*) \quad (12)$$

where:

$$\hat{A}_{k,l,m} = \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \frac{\tilde{A}_k(\theta, \phi)}{\lambda^2} e^{jl\pi \sin(\theta)} e^{-jm\phi} \cos(\theta) d\theta d\phi \quad (13)$$

The discrete approximation for Equation 13 is:

$$\hat{A}_{k,l,m} \approx \frac{4\pi}{N_p N_q} \sum_{q=0}^{N_q} \sum_{p=0}^{N_p} \frac{\tilde{A}_k(\theta_p, \phi_q)}{\lambda^2} e^{jl(\pi \sin(\theta))_p} e^{-jm\phi_q} \quad (14)$$

The matrix form of Equation 13 is:

$$[\tilde{V}_m] = [\hat{A}_m][\tilde{T}_m] \quad (15)$$

Multiple Visibilities

There can be a number of combination of cylinder visibilities that have a non-zero component a given right ascension mode m. However, the sky mode temperature at mode m must be unique.

$$[\tilde{V}_m]^{(1)} = [\hat{A}_m]^{(1)} [\tilde{T}_m] \quad (16)$$

and:

$$[\tilde{V}_m]^{(2)} = [\hat{A}_m]^{(2)}[\tilde{T}_m] \quad (17)$$

To satisfy both equations in a least squares fit, equations 16 and 17 can be combined:

$$\begin{aligned} \left\{ \left\{ [\hat{A}_m]^{(1)} \right\}^T \right\}^* [\tilde{V}_m]^{(1)} + \left\{ \left\{ [\hat{A}_m]^{(2)} \right\}^T \right\}^* [\tilde{V}_m]^{(2)} \\ = \left(\left\{ \left\{ [\hat{A}_m]^{(1)} \right\}^T \right\}^* [\hat{A}_m]^{(1)} + \left\{ \left\{ [\hat{A}_m]^{(2)} \right\}^T \right\}^* [\hat{A}_m]^{(2)} \right) [\tilde{T}_m] \end{aligned} \quad (18)$$